Table X. Experimental Distribution Coefficients D_i of Water (i = 1) and 2-Propanol (i = 2) and Separation Factors $(S = D_2/D_1)^a$

system no.	D2	<i>D</i> ₁	S	
1	3.647	0.127	28.72	
2	3.612	0.128	28.20	
3	0.477	0.023	20.74	
4	2.442	0.284	8.60	
5	1.832	0.283	6.47	
6	2.535	0.134	11.53	
7	2.398	0.150	15.97	
8	0.510	0.019	26.84	
9	3.495	0.089	39.27	

^aComposition range: 10 - 20 wt % of 2-propanol in water.

The results are listed in Table X.

Conclusions

A survey of the literature indicates that no LLE data are available for the present ternaries, except the water + 2propanol + 1,2-dichloroethane system. Our tie-line data are in fair agreement, but the binodal curve compares well with those reported by Izmailov and Franke (1).

It appears that ternaries 4-7 represent type IC systems, whereas 1, 2, and 8 are considered type IB systems. Besides, ternaries 3 and 9 seem to be in the IC category rather than IB (2).

Unfortunately, in the determination of mutual solubilities for IC systems there is some loss of accuracy up to 50% in weight fraction of dissolved component.

It can be mentioned that no solutropic system was observed among the studied ternaries.

Industrial purposes usually require D_i values higher than 0.2 and separation factors higher than 10 (3, 4). Therefore, the studied solvents may serve as separating agents for 2-propanol, except phenylmethanol, cyclohexanol, and 1-pentanol. The best results were obtained with dibenzyl ether and octanenitrile. Unfortunately, these are toxic and expensive solvents. Outstanding advantages of high-boiling solvents in separating substances from dilute aqueous solutions have recently been reported by some researchers (5-8). The solute will be the only overhead product if the solvent has a higher boiling point. With higher solvent/solute ratios, the energy consumption of stripping or distillation operations will be quite high if the solvent has a lower boiling point. Therefore, high-boiling solvents like 2methylbutyl acetate and 1-methylcyclohexanol, showing very low solubility against water, are considered adequate separating agents for 2-propanol.

Glossary

- W_i weight percent of /th component
- W, weight fraction of /th component
- D, distribution coefficient of /th component, eq 1
- S separation factor, eq 2

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Equilibrium Diagrams at 20 °C of Water-Tartaric Acid-2-Methyl-1-propanol, Water-Tartaric Acid-1-Pentanol, and Water-Tartaric Acid-3-Methyl-1-butanol Ternary Systems

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The purpose of this work is to study the tartaric acid recovering possibilities from wine distillery wastewater through a liquid-liquid extracting process. 2-Methyl-1-propanol, 1-pentanol, and 3-methyl-1-butanol may be suitable as extracting solvents. Water-tartaric acid-alcohol ternary system solubility diagrams and tie lines were established at the temperature of 20 °C. Partition coefficients are comprised between 0.07 and 0.42. 1-Pentanol seems to be the best solvent to extract tartaric acid from regeneration of ion-exchanging resins.

Introduction

Tartaric acid is extracted from natural substances. It is an organic acid used as an acidulant in the food processing and pharmaceutical industries (1). In order to recover tartaric acid from wine distillery wastewater, which is present with a concentration of about 3.4 g/L (2, 3), we considered the possibility of using the liquid-liquid extracting process.

The solvation character of oxygen atoms tied to the carbon chain lends especially to alcohols extracting properties with regard to acids. Thus we have selected 2-methyl-1-propanol, 1-pentanol, and 3-methyl-1-butanol.

Experimental Section

Chemicals. The solvents have been obtained with a purity of 98% (mass %) and the tartaric acid with a purity of 99% (mass %). The analysis by the high-performance liquid chromatography method bears out these purities.

Experimental Procedures. Solubility isotherms and tie-line data were determined with an experimental device comprising separatory funnels maintained at the constant temperature of 20 ± 0.1 °C in a thermostated vessel. Several tartaric acid solutions at different concentrations were prepared to determine the tie lines.

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Table I.	Ternary	Diagram	for '	Water	(A)-Tartaric	Acid
(B)-2-M	ethyl-l-pr	opanol (C	C) at	20 °C		

(a) Binodal Curve Data, mass %						
water		tai	rtaric ac	id	2-methy	l-1-propanol
93.3			0.0			6.7
92.2			1.0			6.8
91.1			2.1			6.8
88.6			4.5			6.9
83.4			9.7			6.9
78.5			14.6			6.9
73.6			19.2			7.2
68.7			24.1			7.2
64.0			28.7			7.3
59.4			33.3			7.3
55.0			37.6			7.4
51.1			41.4			7.5
46.0			46.4			7.6
42.8			49 .3			7.9
38.8			53.1			8.1
17.9			22.8			59.3
17.3			19.7			63.0
17.2			16.1			66.7
17.1			8.2			74.7
16.8			3.8			79.4
16.6			1.7			81.7
16.5			0.3			83.2
16.1			0.1			83.8
16.0			0.0			84.0
	(b)	Mutual S	Solubilit	v Data. n	ass %	
water	• •	tar	taric ac	id	2-methy	l-1-propanol
42.8			57.2			0
42.7			56.3			1.0
42.8			54.2			3.0
41.5			52.5			6.0
39.3			52.9			7.8
15.0			20.0			65.0
12.1			17.1			70.8
7.9			13.0			79.1
7.0			11.8			81.2
0			3. 9			96.1
		(c) Tie-l	Line Da	ta, mass '	%	
aqueo	us pha	se (R)	alco	holic pha	se (E)	
X _A	XB	$X_{\rm c}$	XA	X _B	Xc	m
91.1	2.1	6.8	16.5	0.3	83.2	0.14
88.6	4.5	6.9	16.5	0.8	82.7	0.18
73.6	19.2	7.2	16.8	3.8	79.4	0.20
68.7	24.1	7.2	16.8	5.1	78.1	0.21
59.4	33.3	7.3	17.1	8.2	74.7	0.25
55.0	37.6	7.4	17.1	10.6	72.3	0.28
46.0	46.4	7.6	17.2	16.1	66.7	0.35
42.8	49.3	7.9	17.3	19.7	63.0	0.40
38.8	53.1	8.1	17.9	22.8	59.3	0.43
The colu	tione	were m	ived in	alaes-et	onnered	constatory

The solutions were mixed in glass-stoppered separatory funnels and then added to the solvent and shaken for 3 h. That the times allowed for the acid solute distribution equilibrium point and the amount of shaking were sufficient to establish equilibrium was proved by showing that increasing each did not alter the results. After decantation and after another 30 min had passed, tartaric acid, present in the phases in equilibrium, was neutralized with standard sodium hydroxide (0.1 or 1.0 M) and phenolphtalein used as indicator.

The amount of water in each phase at equilibrium was determined by the Karl-Fisher method. The error induced on tie-line compositions based upon five readings is less than 1% $(X \pm 0.01X)$. Solid-liquid saturation curves were determined from saturated solutions, tartaric acid being titrated with standard sodium hydroxide (0.1 or 1.0 M).

Results and Discussion

Figures 1–3 were set at 20 °C from the data of Tables I–III. These figures represent solubility isotherms and tie-line curves



Figure 1. Water-tartaric acid-2-methyl-1-propanol phase diagram with tie lines at 20 °C: S = solid; L = liquid.



Figure 2. Water-tartaric acid-1-pentanol phase diagram with the lines at 20 °C: S = solid; L = liquid.



Figure 3. Water-tartaric acid-3-methyl-1-butanol phase diagram with tie lines at 20 °C: S = solid; L = liquid.

of water-tartaric acid ternary systems with successive solvents: 2-methyl-1-propanol, 1-pentanol, and 3-methyl-1-butanol. The three figures present a zone showing the solid phase, which corresponds to the type 4 classification proposed by Treybal

Table II. Ternary Diagram for Water (A)-Tartaric Acid (B)-1-Pentanol (C) at 20 °C

(a) Binodal Curve Data, mass %						
	water	tar	taric acid		1-pentan	ol
	98.2		0.0		1.8	
	93.5		4.7		1.8	
	88.4		9.7		1.9	
	82.9		14.9		2.2	
	77.8		20.0		2.2	
	73.3		24.6		2.1	
	66.9		30.9		2.2	
	62.9		34.8		2.3	
	57.4		40.3		2.3	
	52.5 40.0		40.3		2.2	
	49.0		48.2		2.2	
	40.7		52.1 57.7		2.2	
	40.0		0/./ 16 E		2.3	
	11.0		10.0		11.1	
	11.0		12.9		70.0	
	11.0		9.0		10.9	
	10.0		0.0 6 7		80.4 89.4	
	10.9		5.9		82.4	
	10.5		4.9		85.3	
	10.0		29		86.7	
	10.3		2.0		87.5	
	10.0		16		88.3	
	99		1.0		89.1	
	9.8		0.4		89.8	
	9.8		0.0		90.2	
	(b) N	(1)+1)al S	alubility	Data m	aaa <i>0</i> 7.	
	water	tor	taric acid	Data, III	1-nenten	
	40.0	tai	57 0		1-pentan	
	42.0		07.2 56 1		0.0	
	42.7		56.5		1.2	
	41.7		57.5		1.0	
	40.5		15.0		2.0 75.1	
	71		12.0		20.1	
	37		93		87.0	
	2.6		72		90.2	
	0.0		5.5		94.5	
		(c) Tie-I	ine Data	mass 9	6 I.C	
80	ueous phase	(R)	alcoh	olic phas	se (E)	
$\frac{-1}{X}$	<u> </u>	<u>X</u>	<u>X.</u>	<u>X-</u>	X.	m
A	47	1.8	<u> </u>		80 8	0.00
82.9	14.9	2.2	10.1	16	88.3	0.05
73.3	24.6	21	10.1	29	86.7	0.12
62.7	34.8	2.5	10.9	5.2	83.9	0.15
52.5	45.3	2.2	11.2	8.6	80.2	0.19
49.6	48.2	2.2	11.4	9.8	78.8	0.20
40.0	57.7	2.3	11.7	16.5	71.8	0.29

(4). The partition coefficient (m) is defined as the ratio of acid concentration (mass percent) in the organic phase to acid concentration (mass percent) in the aqueous phase. Tartaric acid partition coefficients between water and successively 2methyl-1-propanol, 1-pentanol, and 3-methyl-1-butanol for different acid concentrations at 20 °C are indicated in Tables I-III. 2-Methyl-1-propanol presents the most important partition coefficients (0.15 < m < 0.44), whereas 3-methyl-1-butanol presents the lowest partition coefficients (0.07 < m < 0.28).

2-Methyl-1-propanol, which presents the best partition coefficient (Table Ic), is the most soluble in water (Figure 1). 1-Pentanol seems to be the best solvent to extract tartaric acid from effluents resulting from the regeneration of ion-exchanging resins.

Glossary

- XA mass percent of water in one phase
- XB mass percent of tartaric acid in one phase
- Xc mass percent of alcohol in one phase

Table III.	Ternary	Diagrams	for	Water	(A)-Tartaric	Acid
(B)-3-Met	hyl-1-buta	anol (C) at	20	°C		

	(a) Binodal Curve Data, mass %								
_	water		ta	rtaric acio	1	3-meth	yl-1-buta	nol	
	97.5			0.0			2.5		
	94.5			2.9			2.6		
	91.4			6.0			2.6		
	87.6			9.8			2.6		
	82.3			15.0			2.7		
	77.6			19.6			2.8		
	72.4			24.8		2.8			
	67.9			29.1		3.0			
	62.2			34.8			3.0		
	57.1			39.9			3.0		
	52.6			44.3			3.1		
	47.2			50.0			2.8		
	39.6			57.4			3.0		
	11.1			15.9			73.0		
	10.9			8.5			80.6		
	10.4			6.6			83.0		
	10.1			5.3			84.6		
	10.0			4.3			85.7		
	9.9			3.2			86.9		
	9.8			2.4			87.8		
	9.6			1.8			88.6		
	9.4			1.2			89.4		
	9.3			0.8			89.9		
	9.3		0.4 90.3						
	9.0			0.2	.2 90.8				
	8.8			0		91.2			
		(b) N	futual f	Solubility	Data, m	ass %			
	water		ta	rtaric acio	1	3-meth	yl-1-buta	nol	
	42.8			57.2			0.0		
	42.1			56.6			1.3		
	41.4			57.2			1.4		
	40.1			57.0			2.9		
	9.2			14.8			76.0		
	6.3			11.7			82.0		
	6.2			10.9			82.9		
	4.3			8.6			87.1		
	2.9			6.5			90.6		
	0.0			3.9			96.1		
			(c) Tie-	Line Date	a, mass 9	6			
	aqueo	ous phase	e (R)	alcoh	olic phas	se (E)			
	X _A	XB	Xc	X _A	X _B	Xc	m		
	91.4	6.0	2.6	9.3	0.4	90.3	0.07		
	87.6	9.8	2.6	9.3	0.8	89.9	0.08		
	82.3	15.0	2.7	9.4	1.2	89.4	0.08		
	77.6	19.6	2.8	9.6	1.8	88.6	0.09		
	67.9	29.1	3.0	9.9	3.2	86.9	0.11		
	57.1	39.9	3.0	10.1	5.3	84.6	0.11		
	52.6	44.3	3.1	10.4	6.6	83.0	0.15		
	47.2	49.9	2.9	10.9	8.5	80.6	0.17		
	39.6	57.4	3.0	11.1	15.9	73.0	0.28		

Х _{вя}	mass percent of tartaric acid in aqueous pha	se
Х _{ве}	mass percent of tartaric acid in alcoholic pha	ise

- mass percent of water in aqueous phase X_{AR}
- $\boldsymbol{X}_{\mathsf{AE}}$ mass percent of water in alcoholic phase
- partition coefficient m

Registry No. Tartaric acid, 87-69-4; water, 7732-18-5; 2-methyl-1propanol, 78-83-1; 1-pentanol, 71-41-0; 3-methyl-1-butanol, 123-51-3.

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